Comparative Analysis of Transmission Fixed Cost Allocation Methods: Postage Stamp, **Marginal Participation Factors and Power** Tracing

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Abstract - The evolution of deregulated power markets has seen a parallel evolution in transmission pricing methods and philosophies. The methods have evolved from very simple postage stamp method to very elaborate and involved methods like power tracing algorithms. This paper compares the features of three methods viz. Postage Stamp (PS), Marginal Participation Factors (MAPF) and power tracing. These three methods are so chosen that they represent three different principles; cost of unused capacities, sensitivity factors and proportional sharing principle respectively.

Index Terms - Transmission Pricing, Power Tracing, Marginal Participation, Postage Stamp, Sunk cost, Comparison

1 Introduction

N a competitive power market environment, proper Ltransmission pricing scheme, as per FERC guidelines mentioned in order 888 & 889 could meet revenue expectations, promote an efficient operation of electricity markets, encourage investment in optimal locations of generation and transmission lines, and adequately reimburse owners of transmission assets. Most important, the pricing scheme should implement fairness and be practical [1].

However, it is difficult to achieve an efficient transmission pricing scheme that could fit all market structures in different locations [2]. The major part of the cost of the transmission system is fixed cost or sunk cost unlike the generation business. This makes the transmission pricing an even more challenging problem in addition to the challenges posed by the nature of electricity. The amount of research on this issue indicates that there cannot be a single transmission pricing scheme which will satisfy all the criteria discussed so far. Hence gamut of methods are developed on the basis of the characteristics of particular network for which transmission pricing scheme is being designed [3].

The most common and unsophisticated approach which was being used widely in the earlier days of deregulation is postage stamp method. In this method there is no attention paid to the actual system usage and the cost allocation is done on the basis of average system costs.

The user simply pays the charge at a rate equal to a fixed charge per unit of energy transmitted within a particular utility system. What makes this pricing scheme obsolete In addition to this is its inability to accommodate congestion constraints. To introduce fairer and more transparent charges; methods needed to be technically sound and must be able to calculate rates as per actual usage of the system. This encouraged researchers to go for more complex but technically sound methods. One of the very elaborate methods is marginal participation method [4], [5]. This method is based on sensitivity factors of transmission lines and provides locational price signals as well as it can be used to allocate congestion charges.

Another power flow based method is power tracing or average participation method. This was proposed in 1996 almost simultaneously and completely independently by Bialek [6] and Kirschen [7]. Both the approaches are based on proportional sharing principle [8], [9]. Both of these methods determine the contribution of transmission users towards transmission usage. But, both of these methods differ in their approach towards solving the problem. Bialek's method is based on simultaneous equations approach whereas Kirschen's method employs graph theory. Another approach based on graph theory is proposed by Felix Wu [10] which is considered in forthcoming analysis.

2 Methodology Used

2.1 Postage Stamp (PS) Method

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This is a traditionally used method by electricity companies to allocate fixed transmission charges among the users of firm transmission service. This is an embedded cost method or rolled-in cost method. This is the simplest and probably the crudest method as it does not require any power flow calculations and it does not account for the transmission distance and network configuration. The basic assumption of this method is, entire transmission system is used, regardless of the actual facilities that carry the transmission service. The charges are allocated on the basis of average embedded cost and the magnitude of user's transacted power as per equation (1).

$$C_i = TTC \; \frac{P_{Li}}{\sum_{i=1}^n P_{Li}} \tag{1}$$

Where,

 C_i - Charge allocated to $i^{\rm th}$ node, TTC – Total transmission cost, $P_{\rm Li}$ - load in MW at $i^{\rm th}$ bus, n -number of nodes

Apart from its only merit i.e. simplicity this method suffers numerous demerits. This method does not account for the actual system usage and/or congestion in the system. No locational pricing signals are provided by this method. Also, the user at the farthest end of the system is always at benefit since it uses the system most and pays only for the proportion of the load connected at its bus.

2.2 Marginal Participation Factors (MAPF) Method

This is a power flow based method and makes use of sensitivity factors and makes use of extent of use criterion to allocate charges among the system users. This method is also called as "areas of influence" method in Chile and Argentina. The usage is defined as incremental i.e. the incremental change in power flow in each corridor (line) is computed for 1 MW incremental increase in load/generator at each load node. Once the power flow variation in each corridor is obtained for incremental increase in each load/generator the usage index is calculated as per equation (2).

$$U_{il} = \sum_{c, |F_l^i| - |F_l| > 0} (|F_l^i| - |F_l|) P_i$$
(2)

Where, F_i is the base case power flow of the corridor, F_i is the power flow in corridor l when load/generator at ith bus is increased by 1 MW, Pi is the power consumed/generated by ith load/generator resp., U_{il} is the usage factor of ith load over lth corridor.

In this case only positive changes in power flow of a corridor are considered, as this is how it has been implemented traditionally wherever it is used. But, a version can be developed where negative changes in power flow are considered and are paid instead of being charged. This being a marginal method it is necessary to weight each usage factor by amount of load the unit of U^a becomes MW²h.

The marginal participation factor of i^{th} load/generator over l^{th} corridor is given by equation (3).

$$MPF_{il} = \frac{u_{il}}{\sum_{i} u_{il}} \tag{3}$$

This method is dependent on the selection of slack bus to run the power flow. The values of participation factors change once the slack bus is changed. This is applied in Chilean and Argentinean systems where a slack bus is defined and the systems are radial with a strong load in centre and secondly line capacity limits are ignored. Otherwise more advanced technique can be used as given by [11].

2.3 Power Tracing or Average Participation Factors (APF) Method

2.3.1 **Proportional sharing principle**

Both the approaches of power tracing viz. simultaneous equations [6] [12] & graph theoretic [7] [10] are based on the proportional sharing principle. It states that "the nodal inflows are shared proportionally among nodal outflows [8]". Graphically it is illustrated in Fig. 1

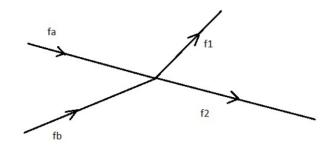


Fig.1 Proportional sharing principle

$$f_{1} = f_{1} \frac{f_{a}}{f_{a} + f_{b}} + f_{1} \frac{f_{b}}{f_{a} + f_{b}}$$
(4)
$$f_{2} = f_{2} \frac{f_{a}}{f_{a} + f_{b}} + f_{2} \frac{f_{b}}{f_{a} + f_{b}}$$
(5)

The assumptions made are,

- Kirchhoff's current law must be satisfied for all the nodes in the network
- Network node is a perfect mixer

2.3.2 Tracing Methods

Power tracing algorithms provide us with,

- Contribution of generators in line flows
- Contribution of loads in line flows
- Load generation interaction
- Loss allocation

The simultaneous equations approach is easy to code but requires distribution matrix inversion and which is very difficult for a large system as distribution matrix can be singular due to its sparse nature. On the other hand graph theoretic approach does not involve matrix inversion and it is very intuitive but it is difficult to code. In the forthcoming discussion graph theoretic approach is used, in particular Wu's method is implemented. Following assumptions are made to simplify the problem,

- An AC load flow solution is available from online state estimation or off-line system analysis
- No loop flows are present
- The line active and reactive power flows keep constant along the line, each edge has a definite direction and the network is lossless.
- A generator has the priority to provide power to the load on the same bus
- The flows of electricity obey the proportional sharing rule

Bus-line incident matrix (BLIM) can be used to form businflow-line (BILIM) and bus-out flow line (BOLIM) incident matrices respectively and determine the pure sink and pure source of the system. A pure source node is that node on which no power inflows exist. A pure sink node is one in which no power outflows exist. This method is also proposed in two versions: upstream looking algorithm and downstream looking algorithm. In this paper downstream looking algorithm is considered. Both the algorithms are dual of each other and give same results. A very lucid explanation and procedure for downstream looking algorithm is given in [13], as follows,

• Start with a node which has highest. This node is called as a pure source. A pure source is defined as a node on which only real power outflows exist and there are no inflows of real power. Delete this node and also remove the lines connected to this node. Carry forward the flows

on these lines to the receiving end nodes as generation contribution of generator on pure source node. Load on this bus is considered as an additional outflow.

- Once the pure source and corresponding lines have been deleted, search for a new pure source. Delete this node and also remove the lines connected to this node. Carry forward the flows on these lines to the receiving end node as generation contribution of generator on pure source node. This is done on proportional sharing basis. Load is considered as an additional outflow on that node
- Repeat this process till all pure sources are exhausted. That means, the nodes which are left are the pure sinks. A pure sink is a node on which only inflows exist. A system can have multiple pure sinks

This downstream tracing (DSTR) algorithm is applied to obtain the contribution factors of individual generators to line flows and loads. The state variable in DSTR is the net generator power. Following matrices are calculated

- Extraction factor matrix of lines and loads from bus total passing power
- The other is contribution factor matrix of generators to bus total passing power

The product of these two matrices constitutes the contribution factors of generators to line flows and loads.

Extraction factors of lines from bus total passing power,

$$P_l = A_l P \tag{6}$$

where, P_1 is the vector of line power, P is the vector of bus passing power in the bus sequence of downstream tracing algorithm & extraction factor matrix of lines Al is calculated as follows

$$(A_l)_{line \ j,bus \ i} = \frac{line \ j'spower \ flow}{bus \ i'stotal \ passing \ power \ P_i}$$
(7)

Similarly, extraction matrix of loads AL is calculated as

$$(A_L)_{ij} = 0$$
 $i \in net \ load \ bus$ (8)

$$=\frac{net \ load \ on \ bus}{P_i} \quad inet \ load \ bus \tag{9}$$

The extraction factor matrix of lines and loads (combined) is obtained as follows

$$A = \begin{bmatrix} A_l \\ A_L \end{bmatrix} \tag{10}$$

IJSER © 2013 http://www.ijser.org The matrix A has one and only one non-zero element in each row and the sum of elements in every column is one.

Contribution factors of generators to bus total passing power,

The contribution factor matrix B is defined as,

$$P = BP_G \tag{11}$$

Where, P_G is the vector of generator power. The matrix B is formed row by row. The elements are calculated as follows

$$B_{bus-i,bus-k} = 1 \quad (k = i, k \in net generation bus)$$

= 0 (k = i, k \net net generation bus)
= 0 (k > i) (12)
= 0 (k < i, k \net net generation bus)
= $\sum_{lj \in i} (A_{lj-m} B_{m-k})$ (k < i, k \in

net generation bus)

Where,

k > i means k is downstream bus of i & hence all corresponding elements are 0 as they do not affect the passing power of the upstream bus.

k < i means k is an upstream bus of i.

lj ϵ i means line j is inflow of bus i.

 A_{ij-m} is the unique nonzero element corresponding to line in matrix Al with bus m as its upstream terminal. B_{m-k} is the element in matrix already calculated which represents the contribution of generator to the total injection power of bus m. The product of above two terms represents the contribution of generator k to the total injection power of bus through line (from bus m to bus k).

The contribution factors of individual generators to line flows and loads are calculated as follows,

$$P_l = A_l P = A_l B P_G = K_{lG} P_G \tag{13}$$

$$P_L = A_L P = A_L B P_G = K_{LG} P_G \tag{14}$$

3 Case Study

Throughout this paper the system taken as a reference is an IEEE 30 bus modified system. All the considered methods are implemented on this modified system presented in Fig. 2. The single line diagram of the system is as follows,

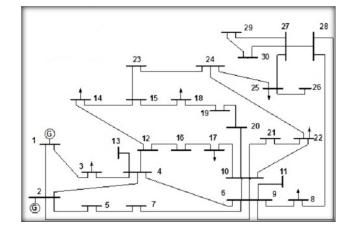


Fig 2 Modified IEEE 30 bus system

The system data is given in appendix D of [8]. The assumptions made are,

- The total sunk cost of the transmission network to be recovered is considered Rs. 10, 00,000/-
- Cost of each line is proportional to its reactance (X)
- Half of the cost will be recovered from loads and half will be from generators
- System is considered as lossless (R is neglected for using DC power flow)
- Only sunk (fixed) cost is considered

4 Results

The nodal charges in Rs/MW obtained after implementing the three discussed methods are as follows

TABLE 1
Nodal charges in Rs/Mw for loads

Load Node	Load (MW)	Average Participation (Power Tracing)	MAPF	PS
2	21.7	45.30526026	32.2777904	1767.40898
3	2.4	374.2589066	1025.10518	1767.40898
4	7.6	271.2383831	390.109863	1767.40898
5	94.2	283.621244	60.5962376	1767.40898
7	22.8	369.3658772	340.551646	1767.40898
8	30	729.5598751	212.295803	1767.40898
10	5.8	1558.218209	3121.54831	1767.40898
12	11.2	615.6378553	859.847744	1767.40898
14	6.2	2715.729016	2819.53908	1767.40898
15	8.2	1884.24221	2055.10014	1767.40898
16	3	2657.807995	5117.4319	1767.40898
17	9	3774.901658	2289.87224	1767.40898

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		1		
18	3.2	4297.404379	6481.0361	1767.40898
19	9.5	4526.905938	2483.21135	1767.40898
20	2.2	3128.9646	11644.3312	1767.40898
21	17.5	1994.068118	1265.24983	1767.40898
23	3.2	4794.920865	7046.79413	1767.40898
24	8.7	8810.708916	3236.94261	1767.40898
26	3.5	10594.66877	15901.6701	1767.40898
29	2.4	6102.877745	25527.7174	1767.40898
30	10.6	9251.238305	8967.79715	1767.40898

TABLE 2 Nodal charges in Rs/Mw for loads

		Average		
Gen	Generatio	Participatio		
Nod	n	n	MAPF	PS
e	(MW)	(Power		
		Tracing)		
1	242.9	944.6723337	1449.5670	1767.4089
1	242.9	944.0723337	2	8
2	40	6232.924747	611.76364	1767.4089
2	40	0232.924747	7	8

TABLE 3 Demand network use rate statistics

	Average		
	Participation	MAPF	PS
	(Power	WATT	15
	Tracing)		
Max (Rs./MW)	10594.67	25527.72	1767.41
Min (Rs./MW)	45.31	32.28	1767.41
Average(Rs./MW)	3275.32	4803.76	1767.41
σ (Rs./MW)	3155.58	6329.71	0.00
Volatility (%)	96.34%	131.77%	0.00%
Cost Recovery Factor (%)	98.29%	95.76%	100.00%

TABLE 4 Generation network use rate statistics

	Average Participation (Power Tracing)	MAPF	PS
Max(Rs./MW)	6232.924747	1449.56702	1767.40898
Min(Rs./MW)	944.6723337	611.763647	1767.40898
Average (Rs./MW)	3588.79854	1030.66533	1767.40898
σ(Rs./MW)	3739.359142	592.416446	0

Volatility (%)	104%	57%	0%
Cost Recovery Factor (%)	96%	75%	100%

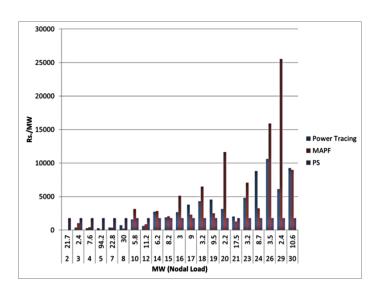


Figure 3. Comparison of nodal charges for loads

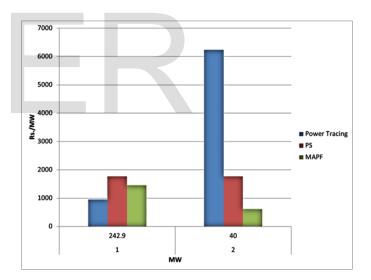


Figure 4. Comparison of nodal charges for generators

5 Conclusion

The system under consideration is characterized by concentration of generation at one end and loads spread throughout the length of the system, hence it is almost a radial system.

From table I and fig. 3 it is observed that the locational price signals are best provided by APF (Power tracing) method as it considers the system usage and nodal demand values, on the other hand MAPF method uses sensitivity of a load/generator for a particular line flow

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and hence the charges vary as per the sensitivity and not the actual usage of system and fail to provide good locational signals. PS method totally fails to provide any kind of locational signals.

From table III, APF method has lesser rate volatility (defined as the ratio of σ and average) for loads as compared to MAPF method whereas table IV shows exactly opposite behaviour in case of generators. Similar contrast is observed in case of σ values in case of loads and generators. This indicates that APF method is a better indicator for network usage with lesser volatility in case of wide spread loads. In PS method no network usage is indicated since system usage is considered on averaged basis which also causes pancaking of charges.

The cost recovery factor (ratio of total cost recovered to total sunk cost) is 100% for postage stamp method but according to DC power flow results line numbers 16 (from bus 12 to bus 13) and 13 (from bus 9 to bus 11) have zero power flow hence zero usage. Hence whether to recover the cost of these unused lines from existing customers or not becomes the policy related issue. But, APF method, being usage based method has less than 100% cost recovery factor indicating that only the cost of actual usage of network has been recovered from existing users. From table III and IV it is evident that APF method is the best method as far as the actual usage based cost recovery is considered. MAPF method has a very poor cost recovery factor for generators.

Hence for a network having similar characteristics to that of considered system APF method is most suitable for fixed cost allocation since it reflects actual network usage, creates moderate price signals, moderate cost recovery and avoids pancaking.

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